## OUTLINE

The R1245x is a Step-down DC/DC converter with internal N -channel high side Tr. That is developed with CMOS process technology. The ON resistance of the built-in high-side transistor is $0.35 \Omega$ and the R1245x can provide the maximum 1.2 A output current. Each of the ICs consists of an oscillator, a PWM control circuit, a voltage reference unit, an error amplifier, a phase compensation circuit, a slope compensation circuit, a soft-start circuit, protection circuits, an internal voltage regulator, and a switch for bootstrap circuit. The ICs can make up a step-down DC/DC converter with an inductor, resistors, a diode, and capacitors. The R1245x is a current mode operating type DC/DC converter without an external current sense resistor, and realizes fast response and high efficiency. As an output capacitor, a ceramic type capacitor can be used with the R1245x. The options of the internal oscillator frequency are preset at 330 kHz for version A and B , 500 kHz for version C and D, 1000 kHz for version E and F, 2400 kHz for version G and H .
As for protection, an Lx peak current limit circuit cycle by cycle, a thermal shutdown function and an under voltage lockout (UVLO) function are built in. Furthermore, there are two types for short protection, for A/C/E/G version, a latch protection function which makes the output latch off if the output voltage keeps lower than the set output voltage for a certain time after detecting current limit is built in, for B/D/F/H version, a fold-back protection function which changes the oscillator frequency slower after detecting short circuit or equivalent. As for the packages of the R1245x, HSOP-8E and DFN2020-8 are available.

## FEATURES

- Input Voltage Range (Maximum Rating) ................... 4.5 V to $30 \mathrm{~V}(32 \mathrm{~V})$

- Internal N-channel MOSFET Driver ......................... Typ. Ron $=0.35 \Omega$
- Adjustable Output Voltage with External Resistor ...... 0.8 V or more

- Peak Current Limit.............................................................. A A
- UVLO Function Released Voltage........................... Typ. 4.0 V
 1000 kHz (E/F version), 2400 kHz (G/H version)
 400 kHz (H version)
- Latch Protection Delay Time ................................. Typ. 4 ms for A/C/E/G version
- Built-in Thermal Shutdown Circuit ...................................... $160^{\circ} \mathrm{C}$
- Ceramic Capacitors Recommended for Input and Output
- Stand-by Current.................................................................... $0 \mu \mathrm{~A}$
- Packages ....................................................................


## R1245x

No. EC-269-200624

## APPLICATIONS

- Power source for car accessories including car audio equipment, car navigation system, and ETC system.
- Power source for control units including EV inverter and charge control.


## SELECTION GUIDE

In the R1245x, the package, type of short protection (Latch or Fold-back), and the oscillator frequency can be selected with the user's request.

## Selection Guide

| Product Name | Package | Quantity per Reel | Pb Free | Halogen Free |
| :---: | :---: | :---: | :---: | :---: |
| R1245S003*-E2-\#E | HSOP-8E | 1,000 pcs | Yes | Yes |
| R1245L003*-TR-AE | DFN2020-8 | 3,000 pcs | Yes | Yes |

*: Designation of the oscillator frequency and the protection function option.

| Symbol | Oscillator Frequency | Latch Protection | Fold-back Protection |
| :---: | :---: | :---: | :---: |
| A | 330 kHz | $\checkmark$ |  |
| B | 330 kHz |  | $\checkmark$ |
| C | 500 kHz | $\checkmark$ |  |
| D | 500 kHz |  | $\checkmark$ |
| E | 1000 kHz | $\checkmark$ |  |
| F | 1000 kHz |  | $\checkmark$ |
| G | 2400 kHz | $\checkmark$ |  |
| H | 2400 kHz |  | $\checkmark$ |

\#: Designated Automotive Class Code

|  | Operating Temperature <br> Range | Guaranteed Specs <br> Temperature Range | Screening |
| :---: | :---: | :---: | :---: |
| A | $-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}$ | $25^{\circ} \mathrm{C}$ | High Temperature |
| J | $-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}$ | $-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}$ | High and low Temperature |

Automotive class code $(A, J)$ varies depending on the package and function.

| Package | Function | Automotive Class Code |  |
| :---: | :--- | :---: | :---: |
|  |  | A | J |
| HSOP-8E | A, B, G, H | $\checkmark$ | $\checkmark$ |
|  | C, D, E, F | $\checkmark$ |  |
| DFN2020-8 | A, B, C, D, E, F, G, H | $\checkmark$ |  |

## BLOCK DIAGRAM



R1245x Block Diagram
*1

| Version | Oscillator Frequency | Short Protection Type |
| :---: | :---: | :---: |
| A | 330 kHz | Latch |
| B | 330 kHz | Fold-back |
| C | 500 kHz | Latch |
| D | 500 kHz | Fold-back |
| E | 1000 kHz | Latch |
| F | 1000 kHz | Fold-back |
| G | 2400 kHz | Latch |
| H | 2400 kHz | Fold-back |

## R1245x

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## PIN DESCRIPTIONS



[^0]R1245L Pin Description

| Pin No. | Symbol | Description |
| :---: | :---: | :--- |
| 1 | Lx | Lx Switching Pin |
| 2 | VIN | Power Supply Pin |
| 3 | VIN | Power Supply Pin |
| 4 | CE | Chip Enable Pin (Active with "H") |
| 5 | GND*2 $^{2}$ | Ground Pin |
| 6 | FB | Feedback Pin |
| 7 | TEST | Test Pin (must be open for user side) |
| 8 | BST | Bootstrap Pin |

[^1]4

INTERNAL EQUIVALENT CIRCUIT FOR EACH PIN


## R1245x

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## ABSOLUTE MAXIMUM RATINGS

| Absolute Maximum Ratings |  |  |  | (GND $=0 \mathrm{~V}$ ) |
| :---: | :---: | :---: | :---: | :---: |
| Symbol | Item | Rating |  | Unit |
| VIN | Input Voltage | -0.3 to 32 |  | V |
| $V_{\text {BST }}$ | BST Pin Voltage | $V_{L X}-0.3$ to $V_{L X}+6$ |  | V |
| VLX | Lx Pin Voltage | -0.3 to $\mathrm{V}_{\mathrm{IN}}+0.3$ |  | V |
| Vce | CE Pin Input Voltage | -0.3 to $\mathrm{V}_{\mathrm{IN}}+0.3$ |  | V |
| $V_{\text {FB }}$ | Feedback Pin Voltage | -0.3 to 6 |  | V |
| PD | Power Dissipation (HSOP-8E) ${ }^{* 1}$ | Ultra High Wattage Land Pattern | 3600 | mW |
|  | Power Dissipation (DFN2020-8)*1 | Standard Land Pattern | 1100 |  |
| Tj | Junction Temperature | -40 to 150 |  | ${ }^{\circ} \mathrm{C}$ |
| Tstg | Storage Temperature Range | -55 to 150 |  | ${ }^{\circ} \mathrm{C}$ |

${ }^{* 1}$ Refer to POWER DISSIPATION for detailed information.

## ABSOLUTE MAXIMUM RATINGS

Electronic and mechanical stress momentarily exceeded absolute maximum ratings may cause the permanent damages and may degrade the lifetime and safety for both device and system using the device in the field. The functional operation at or over these absolute maximum ratings is not assured.

## RECOMMENDED OPERATING CONDITIONS

Recommended Operating Conditions

| Symbol | Item | Rating | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\mathrm{IN}}$ | Input Voltage | 4.5 to 30 | V |
| Ta | Operating Temperature Range | -40 to 105 | ${ }^{\circ} \mathrm{C}$ |

## RECOMMENDED OPERATING CONDITIONS

All of electronic equipment should be designed that the mounted semiconductor devices operate within the recommended operating conditions. The semiconductor devices cannot operate normally over the recommended operating conditions, even if when they are used over such conditions by momentary electronic noise or surge. And the semiconductor devices may receive serious damage when they continue to operate over the recommended operating conditions.

## ELECTRICAL CHARACTERISTICS

$\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$, unless otherwise noted.
The specifications surrounded by $\square$ are guaranteed by design engineering at $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$.

| R1245x003x-AE Electrical Characteristics |  |  |  |  |  | ( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Symbol | Item | Conditions |  | Min. | Typ. | Max. | Unit |
| In | VIN Consumption Current | $\mathrm{V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=1.0 \mathrm{~V}$ |  |  | 0.5 | 1.80 | mA |
| Vuvloi | UVLO Detect Voltage | Falling |  | 3.55 | $\begin{array}{\|c} \hline \text { VUVLO2 } \\ -0.2 \\ \hline \end{array}$ | $\begin{array}{\|l\|l\|} \hline \text { VUVLO2 } \\ -0.05 \\ \hline \end{array}$ | V |
| Vuvloz | UVLO Released Voltage | Rising |  | 3.75 | 4.0 | 4.25 | V |
| $V_{\text {FB }}$ | VFB Voltage Tolerance | $\mathrm{Ta}=25^{\circ} \mathrm{C}$ |  | 0.792 | 0.800 | 0.808 | V |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$ |  | 0.781 |  | 0.819 |  |
| fosc | Oscillator Frequency | Version A/B | $\mathrm{Ta}=25^{\circ} \mathrm{C}$ | 300 | 330 | 360 | kHz |
|  |  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$ | 280 |  | 380 |  |
|  |  | Version C/D | $\mathrm{Ta}=25^{\circ} \mathrm{C}$ | 450 | 500 | 550 |  |
|  |  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$ | 430 |  | 590 |  |
|  |  | Version E/F | $\mathrm{Ta}=25^{\circ} \mathrm{C}$ | 900 | 1000 | 1100 |  |
|  |  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$ | 870 |  | 1140 |  |
|  |  | Version G/H | $\mathrm{Ta}=25^{\circ} \mathrm{C}$ | 2200 | 2400 | 2600 |  |
|  |  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$ | 2150 |  | 2650 |  |
| ffLB | Fold-back Frequency | Version B | $\mathrm{V}_{\mathrm{FB}}<0.56 \mathrm{~V}$ |  | 170 |  | kHz |
|  |  | Version D | $\mathrm{V}_{\text {FB }}<0.56 \mathrm{~V}$ |  | 170 |  |  |
|  |  | Version F | $\mathrm{V}_{\mathrm{FB}}<0.56 \mathrm{~V}$ |  | 250 |  |  |
|  |  | Version H | $\mathrm{V}_{\mathrm{FB}}<0.56 \mathrm{~V}$ |  | 400 |  |  |
| Maxduty | Oscillator Maximum Duty Cycle | Version A/B |  | 91 |  |  | \% |
|  |  | Version C/D |  | 91 |  |  |  |
|  |  | Version E/F |  | 86 |  |  |  |
|  |  | Version G/H |  | 74 |  |  |  |
| tstart | Soft-start Time | $\mathrm{V}_{\mathrm{FB}}=0.72 \mathrm{~V}$ |  |  | 1.0 |  | ms |
| toly | Delay Time for Latch Protection | Version A/G |  |  | 4 |  | ms |

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$\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$, unless otherwise noted.
The specifications surrounded by $\square$ are guaranteed by design engineering at $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$.

R1245x003x-AE Electrical Characteristics $\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$

| Symbol | Item | Conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rıxh | Lx High Side Switch ON Resistance | $\mathrm{V}_{\text {BSt }}-\mathrm{V}_{\text {LX }}=4.5 \mathrm{~V}$ |  | 0.35 |  | $\Omega$ |
| ILXHOFF | Lx High Side Switch Leakage Current | $\mathrm{V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{~V}_{\text {Ce }}=0 \mathrm{~V}$ |  | 0 | 5.0 | $\mu \mathrm{A}$ |
| ILImLxh | Lx High Side Switch Limited Current | $\mathrm{V}_{\text {BSt }}-\mathrm{V}_{\text {LX }}=4.5 \mathrm{~V}$ | 1.2 | 2.0 |  | A |
| $\mathrm{V}_{\text {cel }}$ | CE "L" Input Voltage | $\mathrm{V}_{\text {IN }}=30 \mathrm{~V}$ |  |  | 0.3 | V |
| Vcen | CE "H" Input Voltage | $\mathrm{V}_{\text {IN }}=30 \mathrm{~V}$ | 1.6 |  |  | V |
| $\mathrm{IfB}^{\text {f }}$ | VFB Input Current | $\mathrm{V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=1.0 \mathrm{~V}$ | -0.3 | 0 | 0.3 | $\mu \mathrm{A}$ |
| Icel | CE "L" Input Current | $\mathrm{V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$ | $\bigcirc 0.3$ | 0 | 0.3 | $\mu \mathrm{A}$ |
| Ісен | CE "H" Input Current | $\mathrm{V}_{\text {IN }}=30 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=30 \mathrm{~V}$ | -0.3 | 0 | 0.3 | $\mu \mathrm{A}$ |
| Istandby | Standby Current | $\mathrm{V}_{\text {IN }}=30 \mathrm{~V}$ |  | 0 | 5.0 | $\mu \mathrm{A}$ |

All of units are tested and specified under load conditions such as $\mathrm{Tj} \approx \mathrm{Ta}=25^{\circ} \mathrm{C}$.

V IN $=12 \mathrm{~V}$, unless otherwise noted.

R1245x003x-JE Electrical Characteristics
$\left(-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}\right)$

| Symbol | Item | Conditions |  | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In | VIN Consumption Current | $\mathrm{V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=1.0 \mathrm{~V}$ |  |  | 0.5 | 1.80 | mA |
| Vuvloi | UVLO Detect Voltage | Falling |  | 3.55 | $\begin{gathered} \hline \text { VuvLO2 } \\ -0.2 \end{gathered}$ | $\begin{gathered} \hline \text { VUVLO2 } \\ -0.05 \end{gathered}$ | V |
| Vuvloz | UVLO Released Voltage | Rising |  | 3.75 | 4.0 | 4.25 | V |
| $V_{\text {fb }}$ | VFB Voltage Tolerance | $\mathrm{Ta}=25^{\circ} \mathrm{C}$ |  | 0.792 | 0.800 | 0.808 |  |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$ |  | 0.781 |  | 0.819 |  |
| fosc | Oscillator Frequency | Version A/B | $\mathrm{Ta}=25^{\circ} \mathrm{C}$ | 300 | 330 | 360 | kHz |
|  |  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$ | 280 |  | 380 |  |
|  |  | Version G/H | $\mathrm{Ta}=25^{\circ} \mathrm{C}$ | 2200 | 2400 | 2600 |  |
|  |  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 105^{\circ} \mathrm{C}$ | 2150 |  | 2650 |  |
| ffLb | Fold-back Frequency | Version B | $\mathrm{V}_{\mathrm{FB}}<0.56 \mathrm{~V}$ |  | 170 |  | kHz |
|  |  | Version H | $\mathrm{V}_{\mathrm{FB}}<0.56 \mathrm{~V}$ |  | 400 |  |  |
| Maxduty | Oscillator Maximum. Duty Cycle | Version A/B |  | 91 |  |  | \% |
|  |  | Version G/H |  | 74 |  |  |  |
| tstart | Soft-start Time | $\mathrm{V}_{\mathrm{FB}}=0.72 \mathrm{~V}$ |  |  | 1.0 |  | ms |
| toly | Delay Time for Latch Protection | Version A/G |  |  | 4 |  | ms |
| Rıxh | Lx High Side Switch ON Resistance | $\mathrm{V}_{\text {BSt }}-\mathrm{V}_{\text {LX }}=4.5 \mathrm{~V}$ |  |  | 0.35 |  | $\Omega$ |
| ILXHOFF | Lx High Side Switch Leakage Current | $\mathrm{V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$ |  |  | 0 | 5.0 | $\mu \mathrm{A}$ |
| ILIMLXH | Lx High Side Switch Limited Current | $\mathrm{V}_{\text {BSt }}-\mathrm{V}_{\text {LX }}=4.5 \mathrm{~V}$ |  | 1.2 | 2.0 |  | A |
| $\mathrm{V}_{\text {cel }}$ | CE "L" Input Voltage | $\mathrm{V}_{\text {IN }}=30 \mathrm{~V}$ |  |  |  | 0.3 | V |
| Vcen | CE "H" Input Voltage | V IN $=30 \mathrm{~V}$ |  | 1.6 |  |  | V |
| $\mathrm{I}_{\text {FB }}$ | VFB Input Current | $\mathrm{V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=1.0 \mathrm{~V}$ |  | -0.3 | 0 | 0.3 | $\mu \mathrm{A}$ |
| Icel | CE "L" Input Current | $\mathrm{V}_{\text {IN }}=30 \mathrm{~V}, \mathrm{~V}_{\text {ce }}=0 \mathrm{~V}$ |  | -0.3 | 0 | 0.3 | $\mu \mathrm{A}$ |
| Icen | CE "H" Input Current | $\mathrm{V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{~V}_{\mathrm{CE}}=30 \mathrm{~V}$ |  | -0.3 | 0 | 0.3 | $\mu \mathrm{A}$ |
| Istandby | Standby Current | V IN $=30 \mathrm{~V}$ |  |  | 0 | 5.0 | $\mu \mathrm{A}$ |

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## OPERATING DESCRIPTIONS

## OPERATION OF THE BUCK CONVERTER AND THE OUTPUT CURRENT

The DC/DC converter charges energy in the inductor when the switch turns on, and discharges the energy from the inductor when the switch turns off and controls with less energy loss, so that a lower output voltage than the input voltage is obtained. Refer to the following figures.


Basic Circuit


Current flowing through the Inductor

Step 1: The switch turns on and current IL (= i1) flows, and energy is charged into Cout. At this moment, IL increases from ILmin $(=0)$ to reach ILmax in proportion to the on-time period (ton) of the switch.
Step 2: When the switch turns off, the diode turns on in order to maintain IL at ILmax, and current IL (= i2) flows.
Step 3: IL (= i2) decreases gradually and reaches IL = ILmin = 0 after a time period of topen, and the diode turns off. This case is called as discontinuous mode. If the output current becomes large, next switching cycle starts before IL becomes 0 and the diode turns off. In this case, IL value increases from ILmin (> 0 ), and this case is called continuous mode.

In the case of PWM control system, the output voltage is maintained by controlling the on-time period (ton), with the oscillator frequency (fosc) being maintained constant.

## TYPICAL APPLICATION CIRCUIT



R1245x00xA/B Typical Application Circuit, $330 \mathrm{kHz}, \mathrm{V}_{\text {out }}=1.2 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=\mathbf{2 4} \mathrm{V}$


R1245x00xC/D Typical Application Circuit, $500 \mathrm{kHz}, \mathrm{V}_{\text {out }}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=24 \mathrm{~V}$
*TEST pin must be open.

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R1245x00xE/F Typical Application Circuit, $1000 \mathrm{kHz}, \mathrm{V}_{\text {out }}=3.3 \mathrm{~V} \mathrm{~V}_{\mathrm{IN}}=12 \mathrm{~V}$


R1245x00xG/H Typical Application Circuit, $2400 \mathrm{kHz}, \mathrm{V}_{\text {out }}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=12 \mathrm{~V}$
*TEST pin must be open.

## OUTPUT CURRENT AND SELECTION OF EXTERNAL COMPONENTS

The calculation method of output current and the relation between the output current and external components are as follows:

When the switch of $L x$ turns on:
(Wherein, the peak to peak value of the ripple current is described as $\mathrm{I}_{\mathrm{RP}}$, the ON resistance of the switch is described as Ronh, and the diode forward voltage as $\mathrm{V}_{\mathrm{F}}$, and the DC resistance of the inductor is described as $R_{L}$, and on time of the switch is described as ton)

$$
\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {OUT }}+\left(\mathrm{R}_{\text {ONH }}+\mathrm{R}_{\mathrm{L}}\right) \times \mathrm{lout}+\mathrm{L} \times \mathrm{I}_{\mathrm{RP}} / \text { ton }
$$

Equation 1

When the switch turns off (the diode turns on) as toff:
$\mathrm{L} \times \mathrm{I}_{\mathrm{RP}} /$ toff $=\mathrm{V}_{\mathrm{F}}+\mathrm{V}_{\text {OUT }}+\mathrm{R}_{\mathrm{L}} \times$ Iout
Equation 2

Put Equation 2 to Equation 1 and solve for ON duty of the switch, ton $/(t o f f+$ ton $)=$ Don,

Don $=\left(V_{\text {OUT }}+V_{F}+R_{L} \times\right.$ lout $) /\left(V_{\text {IN }}+V_{F}-\right.$ RoNH $\times$ lout $)$
Equation 3

Ripple Current is as follows:

IRP $=($ VIN - Vout - Ronh $\times$ Iout - RL $\times$ lout $) \times$ Don $/$ fosc $/ L$
Equation 4
wherein, peak current that flows through L, and the peak current ILmax is as follows:

ILmax $=$ lout $+\mathrm{I}_{\mathrm{RP}} / 2$
Equation 5

As for the valley current ILmin,

ILmin $=$ lout $-I_{\text {RP }} / 2$
Equation 6

If ILmin $<0$, the step-down DC/DC converter operation becomes current discontinuous mode.
Therefore the current condition of the current discontinuous mode, the next formula is true.
lout < IRP / 2
Equation 7

Consider ILmax and ILmin, conditions of input and output and select external components.

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## Ripple Current and Lx current limit

The ripple current of the inductor may change according to the various reasons. In the R1245x, as an Lx current limit, Lx peak current limit is used. Therefore the upper limit of the inductor current is fixed.
The peak current limit is not the average current of the inductor (output current). If the ripple current is large, peak current becomes also large. The characteristic is used for the fold-back current limit of version B/D/F/H. In other words, the peak current limit is maintained and the switching frequency is reduced, as a result, the average current of the inductor is reduced. To release this condition, at 170 kHz for version B/D, at 250 kHz for version F , at 400 kHz for version H must not be beyond the peak current limit. In the Figure 1, the sequence of the Lx current limit function is described.


Figure 1. Lx Limit Function Sequence

## Latch protection function for version A/C/E/G

The latch function works after detecting current limit and if the output voltage becomes low for a certain time, the output is latched off. Refer to the TECHNICAL NOTES.

## Fold-back protection function for version B/D/F/H

If FB voltage becomes lower than approximately 0.56 V , the fold-back protection function limits the oscillator frequency to typically 170 kHz for version B/D, typically 250 kHz fir version F , typically 400 kHz for version H . By reducing frequency, the ripple current increases. The R1245x has the peak current limit function, therefore as in the Equation 8, the Lx average current decreases by the increase of the ripple current.
lout $=$ ILmax $+\mathrm{I}_{\mathrm{RP}} / 2$
Equation 8

If FB voltage becomes less than 0.56 V , the oscillator frequency is reduced. At heavy load, if the R1245x becomes into the fold-back protection mode, the situation may not be released by increase the ripple current. In terms of other notes on this protection function, refer to the TECHNICAL NOTES.

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## MAXIMUM OUTPUT CURRENT

The output current of the R1245x is limit by the power dissipation $P_{D}$ of the package and the maximum specification 1.2 A. The loss of the IC includes the switching loss, and it is difficult to estimate. To estimate the maximum output, using the efficiency data is one method.
By using the efficiency data, the loss including the external components can be calculated with the equation, (100/efficiency (\%)-1) x (Vout (V) x lout (A)). From this equation, by reducing the loss of external components, the loss of the IC can be estimated. The main loss of the external components is composed by the rectifier diode and DCR of the inductor. Supposed that the forward voltage of the diode is described as $\mathrm{V}_{\mathrm{F}}$, the loss of the diode can be described as follows:
$\left(\mathrm{V}_{\text {In }}(\mathrm{V})-\operatorname{Ron}_{\text {on }}(\Omega) \times\right.$ lout $\left.(\mathrm{A})-\mathrm{V}_{\text {out }}(\mathrm{V})-\mathrm{V}_{\mathrm{F}}(\mathrm{V})\right)$ ) / $\mathrm{V}_{\text {in }}(\mathrm{V}) \times \mathrm{V}_{\mathrm{F}}(\mathrm{V}) \times$ lout $(\mathrm{A})$
The loss by the DCR of the inductor can be calculated by the formula DCR $(\Omega) \times$ lout $^{2}(A)$.
Thus,
 $\left.\mathrm{V}_{\mathrm{F}}(\mathrm{V})\right) / \mathrm{Vin}^{(\mathrm{V}) \times \mathrm{V}_{\mathrm{F}}(\mathrm{V}) \times \operatorname{lout}(\mathrm{A})-\operatorname{DCR}(\Omega) \times \text { lout }^{2}(\mathrm{~A}), ~(\mathrm{I}}$

The efficiency of the R 1245 x at $\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$, $\mathrm{V}_{\text {OUt }}=3.3 \mathrm{~V}$, lout $=600 \mathrm{~mA}$ is approximately $89.5 \%$ for version $A / B$ (Oscillator frequency 330 kHz ). Supposed that the On resistance of the internal driver is 0.35 $\Omega$, the DCR of the inductor is $65 \mathrm{~m} \Omega$, the $\mathrm{V}_{\mathrm{F}}$ of the rectifier diode is 0.3 V and applied to the formula above, The loss of the $I C=(100 \% / 89.5 \%-1) \times(3.3 \mathrm{~V} \times 0.6 \mathrm{~A})-(12 \mathrm{~V}-0.35 \Omega \times 0.6 \mathrm{~A}-3.3 \mathrm{~V}-0.3 \mathrm{~V}) / 12 \mathrm{~V} \times 0.3 \mathrm{~V}$ $\times 0.6 \mathrm{~A}-0.065 \Omega \times 0.6^{2} \mathrm{~A}=86 \mathrm{~mW}$

The power dissipation $\mathrm{P}_{\mathrm{D}}$ of the package is specified at $\mathrm{Ta}=25^{\circ} \mathrm{C}$ based on the $\mathrm{Tjmax}=150^{\circ} \mathrm{C}$. Thus the thermal resistance of the package $\theta \mathrm{ja}=\left(\operatorname{Tjmax}\left({ }^{\circ} \mathrm{C}\right)-\operatorname{Ta}\left({ }^{\circ} \mathrm{C}\right)\right) / \mathrm{P}_{\mathrm{D}}(\mathrm{W})$, therefore the thermal resistance of the each available package is as follows:
HSOP-8E: $\left(150^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right) / 3.6 \mathrm{~W}=35^{\circ} \mathrm{C} / \mathrm{W}$
DFN2020-8: $\left(150^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right) / 1.1 \mathrm{~W}=114^{\circ} \mathrm{C} / \mathrm{W}$

Due to the loss of the IC is 86 mW for this example, therefore Tj increase of the each package is as follows: HSOP-8E: $35^{\circ} \mathrm{C} / \mathrm{W} \times 86 \mathrm{~mW}=3.01^{\circ} \mathrm{C}$
DFN2020-8: $114^{\circ} \mathrm{C} / \mathrm{W} \times 86 \mathrm{~mW}=9.80^{\circ} \mathrm{C}$

For all the packages, even if the ambient temperature is at $105^{\circ} \mathrm{C}, \mathrm{Tj}$ can be suppressed less than $150^{\circ} \mathrm{C}$. By the increase of the temperature, on resistance and switching loss increases, therefore, temperature margin is not enough, measure the efficiency at the actual maximum temperature and recalculation is necessary.

At the same condition, if the preset frequency is 2400 kHz , the efficiency will be down to approximately $81 \%$. The result of the loss calculation is 310 mW , therefore the Tj increase of each package is as follows:

HSOP-8E: $35^{\circ} \mathrm{C} / \mathrm{W} \times 310 \mathrm{~mW}=10.85^{\circ} \mathrm{C}$
DFN2020-8: $114^{\circ} \mathrm{C} / \mathrm{W} \times 310 \mathrm{~mW}=35.34^{\circ} \mathrm{C}$

All packages can be used at the ambient temperature $105^{\circ} \mathrm{C}$. However as for DFN2020-8 package, be sure to note the power dissipation when using at 2400 kHz since its temperature margin is not sufficient when Tjmax $=150^{\circ} \mathrm{C}$. The following graphs are the output current and estimated ambient temperature limit.


Maximum Output Current


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## SHUTDOWN BY INPUT VOLTAGE CONTROL

If the set output voltage is more than UVLO detector threshold (Typ. 3.8 V ) and on/off control is made by Vin voltage-e.g. in the case of Vin pin and CE pin are connected -, when the circuit is shutdown, the relation between input and output may be beyond the specified maximum duty cycle. If the ratio of input and output is beyond the maximum duty cycle, switching operation stops and the output voltage goes down, but depending on the $\mathrm{V}_{\mathrm{I}}$ decreasing speed, the ratio of $\mathrm{V}_{\mathrm{I}}$ and Vout could become equal or less than the maximum duty cycle, as a result, the output may be resumed and fluctuate. Further, if the input voltage goes down faster than the output voltage as shown in Figure 2, large reverse current may flow. In order to avoid the conditions above, or to maintain the input voltage being larger than the output voltage in the power off process, set CE signal "L" while the input voltage is enough larger than the output voltage, or add a discharge circuit.


Figure 2. Conditions for Reverse Current Generation at Shutdown by Input Voltage Control

## TECHNICAL NOTES

- External components must be connected as close as possible to the ICs and make wiring as short as possible. Especially, the capacitor connected in between Vin pin and GND must be wiring the shortest. If their impedance is high, internal voltage of the IC may shift by the switching current, and the operating may be unstable. Make the power supply and GND lines sufficient. In the wiring of the power supply, GND, Lx, Vout and the inductor, large current by switching may flow. To avoid the bad influence, the wiring between the resistance, "Rup" for setting the output voltage and loading, and the wiring between the inductor and loading must be separated.
- The ceramic capacitors have low ESR (Equivalent Series Resistance) and recommended for the ICs. The recommendation of $\mathrm{C}_{\mathrm{in}}$ capacitor between $\mathrm{V}_{\mathrm{in}}$ and $G N D$ is $10 \mu \mathrm{~F}$ or more for $\mathrm{A} / \mathrm{B} / \mathrm{C} / \mathrm{D}$ version, 4.7 $\mu \mathrm{F}$ or more for E/F version, and $2.2 \mu \mathrm{~F}$ or more for $\mathrm{G} / \mathrm{H}$ version. Verify the bias dependence and the temperature characteristics of the ceramic capacitors. Recommendation conditions are written based on the case which the recommendation parts are used with the R1245x.
- The R1245x is designed with the recommendation inductance value and ceramic capacitor value and phase compensation has been made. If the inductance value is large, due to the lack of current sensing amount of the current mode, unstable operation may result. On the contrary, if the inductance value is small, the current sensing amount may increase too much, low frequency oscillation may occur when the on duty ratio is beyond $50 \%$. Not only that, if the inductance value is small, according to the increase of the load current, the peak current of the switching may increase, as a result, the current may reach the current limit value and the current limit may work.
- As for the diode, use the Schottky diode with small capacitance between terminals. The reference characteristic of the capacitance between terminals is around 100 pF or less at 10 V . If the capacitance between terminals is large, excess switching current may flow and the operation of the IC may be unstable. If the capacitance between terminals of the Schottky diode is beyond 100 pF at 10 V or unknown, verify the load regulation, line regulation, and the load transient response.
- Output voltage can be set by adjustment of the values of R1 and R2. The equation of setting the output voltage is $V_{\text {out }}=V_{F B} \times(R 1+R 2) / R 2$. If the values of $R 1$ and $R 2$ are large, the impedance of $F B$ pin increases, and pickup the noise may result. The recommendation value range of R 2 is approximately between $1.0 \mathrm{k} \Omega$ to $16 \mathrm{k} \Omega$. If the operation may be unstable, reduce the impedance of $F B$ pin.
- For the CE pin, as an ESD protection element, a diode to $\mathrm{V}_{\text {IN }}$ pin is formed internal of the IC. If CE pin voltage may become higher than $\mathrm{V}_{\text {IN }}$ pin voltage, to prevent flowing large current from CE pin to $\mathrm{V}_{\mathrm{IN}}$ pin, connect $10 \mathrm{k} \Omega$ or more resistor between CE and Vin pin.
- Connect the backside heat radiation tab to the GND. As for multi-layered boards, to make better power dissipation, putting some thermal vias on the thermal tab in the land pattern and radiation of the heat to another layer is effective.
- After the soft-start operation, the latch function is enabled for version $A / C / E / G$. The latch protection starts the internal counter when the internal current limit protection circuit detects the current limit. When the internal counter counts up to the latch timer limit, typically 4 ms , the output is latched off. To reset the latch function, make the CE pin "L", or make $\mathrm{V}_{\text {IN }}$ pin voltage lower than UVLO detector threshold. Then in the case that the output voltage or FB voltage becomes setting voltage within the latch timer preset time, counter is initialized. If the slew rate of the power supply is too slow and after the soft-start time, the output voltage does not reach the set output voltage even if the latch timer preset time is over, the latch function may work unexpectedly.


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- After the soft-start operation, fold-back protection function is enabled for version B/D/F/H. The fold-back function will limit the oscillator frequency if the FB pin voltage becomes lower than typically 0.56 V . For B/D version, the oscillator frequency will be reduced typically into 170 kHz , for F version, into 250 kHz , for H version, into 400 kHz.
- If the slew rate of the power supply is too slow, and even after the soft-start time, the output voltage is still less than $70 \%$ of the set output voltage, or FB pin voltage is less than typically 0.56 V , then this function may work unexpectedly.
- The performance of power circuit using this IC largely depends on external components. Selection of external components is very important, especially, do not exceed each rating value (voltage/current/power).

Recommended Values for Each Output Voltage
R1245x003A/B: 330 kHz

| Vout (V) | 0.8 to 1.2 | 1.2 to 2.5 | 2.5 to 5.0 | $5.0 \leq$ |
| :---: | :---: | :---: | :---: | :---: |
| R1 (Rup) (k) | $=($ Vout $/ 0.8-1) \times \mathrm{R} 2$ |  |  |  |
| R 2 ( $\mathrm{R}_{\text {вот }}$ ) ( k ) ) | 16 | 12 | 1.20 | 1.20 |
| $\mathrm{C}_{\text {SPD }}$ (pF) | open | 470 | 2200 | 1000 |
| Cout ( $\mu \mathrm{F}$ ) | 47 | 47 | 22 | 22 |
| $\mathrm{L}(\mu \mathrm{H})$ | 4.7 | 10 | 15 | 33 |

R1245x00xC/D: 500 kHz

| Vout (V) | 0.8 to 1.2 | 1.2 to 1.5 | 1.5 to 2.0 | 2.0 to 5.0 | 5.0 to 12.0 | $12.0 \leq$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1 (Rup) (k ${ }^{\text {a }}$ ) | $=($ Vout $/ 0.8-1) \times \mathrm{R} 2$ |  |  |  |  |  |
| R 2 (Rвот) ( $k$ ) | 16 | 16 | 16 | 1.2 | 1.2 | 1.2 |
| Cspd (pF) | open | 100 | 100 | 1000 | 1000 | 470 |
| Cout ( $\mu \mathrm{F}$ ) | 100 | 100 | 22 | 22 | 22 | 22 |
| L ( $\mu \mathrm{H}$ ) | 4.7 | 4.7 | 10 | 10 | 15 | 15 |

R1245x00xE/F: 1000 kHz

| Vout (V) | 0.8 to 1.0 | 1.0 to 1.2 | 1.2 to 1.5 | 1.5 to 2.5 | 2.5 to 5.0 | $5.0 \leq$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1 (Rup) (k ${ }^{\text {) }}$ | $=\left(\mathrm{V}_{\text {Out }} / 0.8-1\right) \times \mathrm{R} 2$ |  |  |  |  |  |
| R2 (Rвот) (k 2 ) | 16 | 16 | 16 | 16 | 1.2 | 1.2 |
| $\mathrm{C}_{\text {spd }}(\mathrm{pF})$ | open | 100 | 100 | 100 | 470 | 470 |
| Cout ( $\mu \mathrm{F}$ ) | 100 | 100 | 47 | 22 | 10 | 10 |
| L ( $\mu \mathrm{H}$ ) | 2.2 | 2.2 | 2.2 | 2.2 | 4.7 | 10 |

R1245x003G/H: 2400 kHz

| Vout (V) | 1.5 to 1.8 | 1.8 to 2.5 | 2.5 to 5.0 | $5.0 \leq$ |
| :---: | :---: | :---: | :---: | :---: |
| R1 (Rup) (k ${ }^{\text {) }}$ | $=\left(\mathrm{V}_{\text {Out }} / 0.8-1\right) \times \mathrm{R} 2$ |  |  |  |
| R 2 ( $\mathrm{R}_{\text {вот }}$ ) ( k ) | 16 | 12 | 1.2 | 1.2 |
| Cspd (pF) | 100 | 100 | 470 | 470 |
| Cout ( $\mu \mathrm{F}$ ) | 10 | 10 | 4.7 | 4.7 |
| L ( $\mu \mathrm{H}$ ) | 1.0 | 1.5 | 2.2 | 4.7 |

## Divider Resisters Values and Possible Setting Range of Input /Output

| Vout <br> [V] | $\begin{aligned} & \text { R1 (Rup) } \\ & {[k \Omega]} \end{aligned}$ | $\begin{gathered} \text { R2 (Rвот) } \\ {[\mathrm{k} \Omega]} \end{gathered}$ | Input Voltage Range [V] |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Ver. AB | Ver. CD | Ver. EF | Ver. GH |
| 0.8 | 0 | open | 4.5 to 20 | 4.5 to 13.5 | 4.5 to 7 | - |
|  | 0 | 16 |  |  |  |  |
| 1 | 4 | 16 | 4.5 to 25.5 | 4.5 to 17 | 4.5 to 8.5 | - |
| 1.2 | 8 | 16 | 4.5 to 30 | 4.5 to 20 | 4.5 to 10 | - |
|  | 6 | 12 |  |  |  |  |
| 1.5 | 10.5 | 12 | 4.5 to 30 | 4.5 to 25 | 4.5 to 12.5 | 4.5 to 5.5 |
|  | 14 | 16 |  |  |  |  |
| 1.8 | 20 | 16 | 4.5 to 30 | 4.5 to 30 | 4.5 to 15 | 4.5 to 6.5 |
|  | 15 | 12 |  |  |  |  |
| 2 | 24 | 16 | 4.5 to 30 | 4.5 to 30 | 4.5 to 17 | 4.5 to 7 |
|  | 1.8 | 1.2 |  |  |  |  |
| 2.5 | 34 | 16 | 4.5 to 30 | 4.5 to 30 | 4.5 to 21 | 4.5 to 9 |
|  | 25.5 | 12 |  |  |  |  |
|  | 2.55 | 1.2 |  |  |  |  |
| 3.3 | 3.75 | 1.2 | 4.5 to 30 | 4.5 to 30 | 4.5 to 27.5 | 4.5 to 12 |
| 5 | 6.3 | 1.2 | 5.5 to 30 | 5.5 to 30 | 6 to 30 | 7 to 18.5 |
| 6 | 7.8 | 1.2 | 6.5 to 30 | 6.5 to 30 | 7 to 30 | 8 to 20 |
| 9 | 12.3 | 1.2 | 10 to 30 | 10 to 30 | 11 to 30 | 12 to 30 |
| 12 | 16.8 | 1.2 | 13 to 30 | 13 to 30 | 14 to 30 | 16 to 30 |
| 15 | 21.3 | 1.2 | 16.5 to 30 | 16.5 to 30 | 17 to 30 | 20 to 30 |
| 24 | 34.8 | 1.2 | 26.5 to 30 | 26.5 to 30 | 27.5 to 30 | 30 |

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Recommended External Components Examples (Considering all the range)

| Symbol | Condition | Value | Parts Name | MFR |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Cin}^{\text {a }}$ | 50 V/X5R <br> 50 V/ X5R <br> 50 V/X7R <br> 50 VIX7R | $\begin{aligned} & \hline 10 \mu \mathrm{~F} \\ & 10 \mu \mathrm{~F} \\ & 4.7 \mu \mathrm{~F} \\ & 2.2 \mu \mathrm{~F} \end{aligned}$ | UMK325BJ106MM-P CGA6P3X7S1H106K GRM31CR71H475KA12L GRM31CR71H225KA88L | TAIYO YUDEN TDK muRata muRata |
| Cout | 50 V/X5R <br> $50 \mathrm{~V} / \mathrm{X} 5 \mathrm{R}$ <br> 50 V/X7R <br> 50 VIX7R <br> 25 VIX7R <br> 10 V/X7R <br> 16 V/B <br> 10 V/X7R | $10 \mu \mathrm{~F}$ <br> $10 \mu \mathrm{~F}$ <br> $10 \mu \mathrm{~F}$ <br> $4.7 \mu \mathrm{~F}$ <br> $10 \mu \mathrm{~F}$ <br> $22 \mu \mathrm{~F}$ <br> $47 \mu \mathrm{~F}$ <br> $47 \mu \mathrm{~F}$ | UMK325BJ106MM-P CGA6P3X7S1H106K KTS500B106M55NOT00 GRM31CR71H475KA12L GRM31CR71E106K GRM31CR71A226M GRM32EB31C476KE15 GRM32ER71A476KE15 NOTE: The value of Cout depends upon the set output voltage. | TAIYO YUDEN <br> TDK <br> Nippon Chemi-Con muRata muRata <br> muRata <br> muRata <br> muRata |
| Cbst | $16 \mathrm{~V} / \mathrm{X} 7 \mathrm{R}$ | $0.47 \mu \mathrm{~F}$ | EMK212B7474KD-T | TAIYO YUDEN |
| L | $\begin{aligned} & 1.8 \mathrm{~A} \\ & 1.65 \mathrm{~A} \\ & 1.7 \mathrm{~A} \\ & 2.4 \mathrm{~A} \\ & 1.9 \mathrm{~A} \\ & 2.3 \mathrm{~A} \\ & 1.9 \mathrm{~A} \\ & 1.9 \mathrm{~A} \\ & 1.7 \mathrm{~A} \\ & 1.65 \mathrm{~A} \\ & 1.8 \mathrm{~A} \\ & 1.8 \mathrm{~A} \end{aligned}$ | $10 \mu \mathrm{H}$ <br> $4.7 \mu \mathrm{H}$ <br> $4.7 \mu \mathrm{H}$ <br> $4.7 \mu \mathrm{H}$ <br> $10 \mu \mathrm{H}$ <br> $15 \mu \mathrm{H}$ <br> $22 \mu \mathrm{H}$ <br> $33 \mu \mathrm{H}$ <br> $2.2 \mu \mathrm{H}$ <br> $2.2 \mu \mathrm{H}$ <br> $1.5 \mu \mathrm{H}$ <br> $1.0 \mu \mathrm{H}$ | SLF6045T-100M1R6-3PF <br> SLF7045T-4R7M2R0-PF <br> NR4018T4R7M <br> NR6020T4R7N <br> NR6028T100M <br> NR6045T150M <br> NR6045T220M <br> NR8040T330M <br> VLCF4020T-2R2N1R7 <br> NR4012T2R2M <br> NR3015T1R5N <br> NR4010T1RON | TDK <br> TDK <br> TAIYO YUDEN <br> TAIYO YUDEN <br> TAIYO YUDEN <br> TAIYO YUDEN <br> TAIYO YUDEN <br> TAIYO YUDEN <br> TDK <br> TAIYO YUDEN <br> TAIYO YUDEN <br> TAIYO YUDEN |
| Diode | $\begin{array}{\|l} \hline 30 \mathrm{~V} / 2.0 \mathrm{~A} \\ 40 \mathrm{~V} / 2.0 \mathrm{~A} \end{array}$ | $\begin{aligned} & 0.37 \mathrm{~V} \\ & 0.55 \mathrm{~V} \end{aligned}$ | CMS06 <br> CMS11 | $\begin{aligned} & \hline \text { TOSHIBA } \\ & \text { TOSHIBA } \end{aligned}$ |
| Rce | The Up Diode is connected between the CE pin and the Vin pin as the ESD protection element. If there is the possibility that the voltage of the CE pin becomes higher than the voltage of the Vin pin, it is recommended to connect the $10 \mathrm{k} \Omega$ resistance with the CE pin for preventing a large current flows into the Vin pin from the CE pin. |  |  |  |

## APPLICATION INFORMATION

## TO IMPROVE THE PERFORMANCE

The R1245 can make its performance better, adding components as shown below.

## Cspd: Speed up capacitor

Cspd has two roles, one is to improve the stability, and the other is to improve the transient speed.
The transfer function from Vout (-which is made of Cspd and feedback resisters, R1(Rup) and R2(Rbot)) to FB will make a forward bump by low frequency zero and high frequency pole, and improve the stability of feedback loop. Cspd can improve the gain and make the transient speed fast at high frequency.


Figure 3. Transfer function BODE plot from Vout to $F B(R 1=3.75 \mathrm{k} \Omega, \mathrm{R} 2=1.2 \mathrm{k} \Omega, \mathrm{Cspd}=470 \mathrm{pF}$ )

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## To improve the stability

If the resistance values of the R1 and R2 have to be changed, make the value of R1*Cspd be constant.
(For example, with the $\mathrm{R} 1245 \times 00 \times \mathrm{A} / \mathrm{B}$ and making $\mathrm{V}_{\text {out }}=1.2 \mathrm{~V}$, if $\mathrm{R} 1=0.6 \mathrm{k} \Omega, \mathrm{R} 2=1.2 \mathrm{k} \Omega$ are used, Cspd=4700pF. By making the values of R1 and R2 increase, the impedance of FB pin also increases, as a result, the influence by noise must be cared. To avoid this, recommendation value range of R2 is from $1.0 \mathrm{k} \Omega$ to $16 \mathrm{k} \Omega$. If the operation becomes unstable by increasing the impedance, choose low resistance value.

If Cout and $L$ are necessary to be changed, or unusual voltage setting is necessary, the Cspd value must be adjusted. The instruction of the adjustment is as follows:

1. Without Cspd, measure the output under-shoot amount by load transient response.
2. Further, with using a small value Cspd, measure the output under-shoot amount by load transient response. The appropriate initial value is about $1 / 10$ of the recommendation Cspd value. If Cspd is too small, the under-shoot amount is almost same as the one without Cspd. If the value of Cspd is changed bigger gradually, the under-shoot amount will be less. Supposed that this new good Cspd as Cspd1, and continue to make it bigger, and finally, the under-shoot amount becomes unchanged, at this point, supposed that the maximum Cspd as Cspd2.
3. Select an appropriate value according to the formula, Cspd= $\sqrt{ }($ Cspd1*Cspd2).

## To improve the transient response speed

If the stability is enough, (for example, in the case that Cout is big enough), make Cspd value bigger. The stability will be same, but the gain at high frequency will be large, and improve the transient response speed. However, if Cspd value is set Cspd2 value or more, the result will not be improved, not only that, due to the high gain at high frequency, compared with the result without Cspd, the stability will be worse.
(1)R1 $=3.75 \mathrm{k} \Omega, \mathrm{R} 2=1.2 \mathrm{k} \Omega$, Cspd: none, $\mathrm{V}_{\text {out }}=3.3 \mathrm{~V}$


Due to no Cspd, the stability is not good enough, and under-shoot amount is big during the load transient.
(2) R1 $=3.75 \mathrm{k} \Omega, \mathrm{R} 2=1.2 \mathrm{k} \Omega, \mathrm{Cspd}=2200 \mathrm{pF}, \mathrm{V}_{\text {out }}=3.3 \mathrm{~V}$


Cspd value is appropriate, and stability and response speed is adjusted properly.
(3) $\mathrm{R} 1=3.75 \mathrm{k} \Omega, \mathrm{R} 2=1.2 \mathrm{k} \Omega, \mathrm{Cspd}=33000 \mathrm{pF}, \mathrm{V}$ оut $=3.3 \mathrm{~V}$


Cspd value is too big, the response speed is fast, but the stability decrease slightly.

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## Rspd: Noise reduction filter for speed up capacitor

Cspd can improve the high frequency characteristics due to its differential function. In other words, the high frequency component is passed through without change, therefore the spike noise of Vout is transferred to FB pin as it is. If the spike noise is too big, by its noise of FB pin, the output voltage may be changed especially at heavy load. To avoid this situation, by setting an Rspd which inserts in series in Cspd and making a pole at high frequency, filtering is possible and effective. The appropriate value range of Rspd is from $10 \Omega$ to $30 \Omega$. If the resistance value is too big, the effect of Cspd is cancelled by the lowering pole at high frequency by Rspd. By removing FB pin noise, using low R1 and R2 resistance value.

## VOLTAGE BETWEEN Lx PIN AND BST PIN

In the boot-strap style switching regulator, when the Lx pin voltage becomes lower than the regulator which supplies BST voltage, $\mathrm{C}_{\text {BST }}$ is charged.

By this charge, while the Lx pin voltage is " H ", high side switch can be turned on continuously. Therefore, if Lx pin voltage does not become lower than the BST voltage supply regulator, switching may be abnormal. In the R1245, the output voltage of the BST voltage supply regulator is set at 5 V . The abnormal switching may be caused by the following conditions:

## - $\mathrm{V}_{\text {out }}>5 \mathrm{~V}$, the difference between $\mathrm{V}_{\text {In }}$ and $\mathrm{V}_{\text {out }}$ is small, inductor current is discontinuous by light load

When the inductor current is continuous, or load current is big enough even if the discontinuous mode, the forward current of the diode will make Lx pin voltage down and $\mathrm{C}_{\mathrm{BSt}}$ is charged, but at light load, Lx pin voltage does not become low enough against the BST voltage supply regulator output( 5 V ). The voltage of $\mathrm{C}_{\text {bSt }}$ is not high enough and drive capability will be down. (Figure 4-1) Due to the lack of the drive capability, Vout cannot be maintained, and under-shoot happens to Vout, Lx pin voltage may become lower than the BST voltage supply regulator output ( 5 V ), but the error amplifier operation may be abnormal. When the charge of $\mathrm{C}_{\mathrm{BSt}}$ is recovered and normal switching starts, Vout becomes back to set output voltage. However, after recovering the Vout, to recover the error amplifier's operation, some response time is necessary, during this response time, Vout may be over-shoot. (Figure 4-(2) As a result, Lx pin voltage cannot be low enough against the BST voltage supply regulator output voltage (5V), undershoot and over-shoot may be repeated. (Figure 5)

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Abnormal waveforms are shown in the next figures. Figure 4: Vin voltage start-up is slower than the softstart time Figure 5: The voltage difference between input and output is small and load current is small In both cases, the voltage between Lx pin and BST pin is not enough.


Figure 4. VIN slow start-up (R1245S003A: $V_{I N}=30 \mathrm{~V}$, Vout $_{\text {( }}=24 \mathrm{~V}$, lout $=0 \mathrm{~mA}$ )
Tek


Figure 5. The voltage difference between input and output is small (R1245S003A Vin=5.5V, Vout=5V, lout=500uA)

To avoid these situation, please refer to the countermeasures shown below:

- If start-up with Vout>5V is necessary, avoid the extremely low load, and start up should be done by CE pin control after Vin becomes high enough.
- If $\mathrm{V}_{\text {out }}>5 \mathrm{~V}$ at low load operation is necessary, make the inductance value bigger and assure the "L" time of Lx.
- If start-up with $\bigvee_{\mathbb{I}}=C E$ is necessary, avoid very slow $V_{\mathbb{N}}$ setting and low load current condition.

During the output overshoot while the normal transient response, even the no-switching condition happens, the operation keeps normal. Other than that, low load condition with Vout<5V is also normal condition for the device.

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## MINIMUM ON TIME

The minimum On time of the R1245 is Typ.110ns. 110ns derives from the current sense circuit delay time and stability.

The R1245 has adopted current mode control without an external sense resistance. Instead of the external sense resistance, the on resistance of the N -channel driver: Ron is used. Vin-Vıx=I $\mathrm{I} \times \times$ Ron, therefore Itx (inductor current) can be sensed. Ilx can be sensed during the on time of the N-channel driver, ( $\mathrm{Lx}=\mathrm{H} H \mathrm{H}$ ), if Lx switching surge is sensed just after turning on, the operation may be abnormal, therefore, just after turning on the N -channel driver, sensing is stopped for a short period and avoid the error by the switching surge.
Therefore, during this sensing delay time, current mode control and current limit cannot operate properly.
Figure 6. X-axis: On time, Y-axis: Current limit
By this current sense delay time, 110ns or less, current limit circuit has also delay time, and detecting current increases drastically. This delay time includes the signal delay time from the current sense circuit to the driver.


Figure 6. On time and Lx current limit, Lx pin current peak value Ilxıim
This could be applied to the current mode control. Therefore, 110ns or less, current mode control does not work correctly, and operation becomes like a low stability voltage control mode.
Thus, the R1245 operation less than 110ns, stability and current limit detecting accuracy are deteriorated. If the condition is close to minimum on time, stability must be assured by external components, and over current protection other than the IC is necessary.

## INPUT VOLTAGE TRANSIENT

In the R1245, if the voltage between input and output is small and max. duty condition, or if the input voltage changes from lower than the set output voltage to high voltage rapidly, depending on the setting frequency of the R1245, output voltage may be over-shoot to input voltage.

Figure 7: Output voltage is set at 5 V , and the input voltage is also set at 5 V . The figure shows the input voltage transient response of the input voltage from 5 V to 15 V rapidly. External voltages: General recommendation values on datasheet, load $20 \Omega$ resistance, or 250 mA load current.

In the high switching frequency type, the response speed is excellent, therefore, input transient characteristic is good, and over-shoot is suppressed. If input voltage rapid change must be considered, choose the high frequency type.


Figure 7. Input transient response from low difference voltage between input and output to high voltage

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If the difference between input and output is large, then over-shoot will not happen. In the Figure 8, Other than the start VIN, the conditions are same as Figure 7 . VIN is changed from 8 V to $18 \mathrm{~V}, 330 \mathrm{kHz}$ type, input transient response. Frequency is the lowest, but there is no over-shoot.


Figure 8. Input transient response from the big difference between input and output
To improve the situation shown in Figure 7, as shown in Figure 9, by using a zener diode, ZD and resistance, when the VIN decreases, CE pin is set at " L " and make the IC standby, over-shoot will be suppressed. Because, when the VIN goes up again and IC becomes active, soft-start function will work. If the input voltage, VIN goes down, Before the set output voltage $\mathrm{V}_{\text {SET }}$ against VIN ratio, ( $\mathrm{V}_{\text {SET }} / \mathrm{VIN}$ ) becomes more than the max. duty, CE voltage must be "L". Consider this ratio and choose ZD voltage, or under the ZD, the voltage made by divider resisters must be forced to CE.


Figure 9. Low input voltage countermeasure circuit with using ZD

## THE NOTE OF LAYOUT PATTERN

1. The wire of Power line ( $\mathrm{V}_{\mathrm{IN}}, \mathrm{GND}$ ) should be broad to minimize the parasitic inductance. The Bypass capacitor (Cin) must be connected as close as possible in between Vin - GND.
2. The wire between Lx pin and the inductor as short as possible to minimize the parasitic inductance.

This evaluation board is designed for the product evaluation board. Therefore large inductors or diodes can be set and the large space of Lx area has been secured. The evaluation board, R1245L003x ( 2400 kHz ) with the reduced mounting area including external components, is available due to the small package of R1245L003G/H and the low recommended constant numbers including inductors.
3. The ripple current flows through the output capacitor. If the GND side of the output capacitor is connected very close to GND pin of the IC, the noise might have a bad impact on the IC. Therefore, the GND side of the output capacitor is better to connect to the outside of the GND of the $\mathrm{C}_{\mathrm{IN}}$, or connect to the GND plain layer.
4. Rup, Rbot, Cspd, and Rspd should be mounted on the position as close as possible to the FB pin, and away from the inductor and BST pin.
5. The feed-back must be made as close as possible from the Output capacitor (Cout).

## PCB LAYOUT

R1245S003x


## R1245x

No. EC-269-200624

R1245L003x


R1245L003x ( 2400 kHz )


## TYPICAL CHARACTERISTICS

Note: Typical Characteristics are intended to be used as reference data; they are not guaranteed.

1) FB voltage vs. Temperature

R1245x00xx

2) Driver On resistance vs. Temperature

R1245x00xx
$\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right)$

3) Oscillator frequency vs. Temperature


R1245x00xER1245x00xF




## R1245x

No. EC-269-200624
4) Maximum duty cycle vs. Temperature




5) Fold-back frequency vs. Temperature


6) High side switch current limit vs. Temperature


R1245x00xD


R1245x00xH


## R1245x

No. EC-269-200624
7) UVLO detector threshold vs. Temperature

9) Soft-start time vs. Temperature

R1245x00xx

11) $C E$ " $H$ " Input voltage vs. Temperature R1245x00xx

8) UVLO released voltage vs. Temperature

10) Timer latch delay vs. Temperature

R1245x00xx

12) $C E$ "L" Input voltage vs. Temperature

R1245x00xx

13) Soft-start waveform

R1245x00xA/R1245x00xB

$$
\text { Vout }=3.3 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V} \text {, ІІut }=0 \mathrm{~mA}, \mathrm{Ta}=25^{\circ} \mathrm{C}
$$


14) Switching operation waveform

R1245x00xA/R1245x00xB
Vout $=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{in}}=12 \mathrm{~V}$, lout $=0 \mathrm{~mA}, \mathrm{Ta}=25^{\circ} \mathrm{C}$


2 $\mu \mathrm{s} / \mathrm{div}$
R1245x00xG/R1245x00xH
$\mathrm{V}_{\text {OUt }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}$, lout $=20 \mathrm{~mA}, \mathrm{Ta}=25^{\circ} \mathrm{C}$


R1245x00xA/R1245x00xB
Vout $=3.3 \mathrm{~V}, \mathrm{~V}_{\text {In }}=\mathbf{1 2} \mathrm{V}$, lout $=\mathbf{6 0 0} \mathrm{mA}, \mathrm{Ta}=25^{\circ} \mathrm{C}$


R1245x00xA/R1245x00xB
Vout $=3.3 \mathrm{~V}$, $\mathrm{V}_{\text {in }}=12 \mathrm{~V}$, Іоит $=600 \mathrm{~mA}, \mathbf{T a}=\mathbf{2 5}{ }^{\circ} \mathrm{C}$

$2 \mu \mathrm{~s} / \mathrm{div}$
R1245x00xG/R1245x00xH
$\mathrm{V}_{\text {OUt }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}$, lout $=600 \mathrm{~mA}, \mathrm{Ta}=25^{\circ} \mathrm{C}$


## R1245x

No. EC-269-200624
15) Load transient response waveform

R1245x00xA/R1245×00xB
$V_{\text {out }}=0.8 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}$, lout $=600 \Leftrightarrow 1200 \mathrm{~mA}, \mathbf{T a}=25^{\circ} \mathrm{C}$

$100 \mu \mathrm{~s} / \mathrm{div}$

## R1245x00xG/R1245x00xH



50us/div

R1245x00XA/R1245x00xB
$V_{\text {out }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}$, lout $=600 \Leftrightarrow 1200 \mathrm{~mA}, \mathbf{T a}=25^{\circ} \mathrm{C}$

$100 \mu \mathrm{~s} / \mathrm{div}$

## R1245x00xG/R1245x00xH

$V_{\text {OUt }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}$, lout $=600 \Leftrightarrow 1200 \mathrm{~mA}, \mathrm{Ta}=25^{\circ} \mathrm{C}$

## Vout <br> ( $100 \mathrm{mV} / \mathrm{div}$ )

lout
( $500 \mathrm{~mA} / \mathrm{div}$ )


50us/div
16) Limit latch operation waveform R1245x00xA

Vout $=3.3 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}$, Rout $=5.5 \Omega \rightarrow 0.05 \Omega, \mathrm{Ta}=25^{\circ} \mathrm{C}$

18) Fold-back operation waveform

R1245x00xB
VOUT $=3.3 \mathrm{~V}, \mathrm{VIN}=12 \mathrm{~V}$, ROUT $=5.5 \Omega \rightarrow 0.05 \Omega, \mathrm{Ta}=25^{\circ} \mathrm{C}$
17) Released waveform from limit latch

R1245x00xA
Vout $=3.3 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}$, Rout $=5.5 \Omega \rightarrow 0.05 \Omega \rightarrow 5.5 \Omega$

19) Released waveform from fold-back

R1245x00xB
Vout $=3.3 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}$, Rout $=5.5 \Omega \rightarrow 0.05 \Omega \rightarrow 5.5 \Omega$
$\mathrm{Ta}=25^{\circ} \mathrm{C}$


20 $\mu \mathrm{s} / \mathrm{div}$
20) Switching waveform at fold-back operation R1245x00xB


## R1245x

No. EC-269-200624
21) Output current vs. Efficiency (Version A/B)


R1245x00xA/R1245x00xB
Vout=5.0V
(Ta=25 ${ }^{\circ} \mathrm{C}$ )


R1245x00xA/R1245x00xB
Vout=15V


R1245x00xA/R1245x00xB
Vout=3.3V
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$


R1245x00xA/R1245x00xB
Vout $=12 \mathrm{~V}$
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$


R1245x00xA/R1245x00xB
Vout $=24 \mathrm{~V}$

22) Output Current vs. Efficiency (Version C/D)


R1245x00xC/R1245x00xD
Vout=5.0V


R1245x00xC/R1245x00xD
Vout $=15 \mathrm{~V}$


R1245x00xC/R1245x00xD
Vout=3.3V


R1245x00xC/R1245x00xD
Vout $=12 \mathrm{~V}$


R1245x00xC/R1245x00xD
Vout $=24 \mathrm{~V}$


## R1245x

No. EC-269-200624
23) Output current vs. Efficiency (Version E/F)


R1245x00xE/R1245x00xF
Vout=5.0V


R1245x00xE/R1245x00xF
Vout $=15 \mathrm{~V}$


R1245x00xEIR1245x00xF
Vоut=3.3V
( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


R1245x00xEIR1245x00xF
Vout $=12 \mathrm{~V}$


R1245x00xEIR1245x00xF
Vout $=24 \mathrm{~V}$


## 24) Output current vs. Efficiency (Version G/H)





## R1245x

No. EC-269-200624
25) Output current vs Output voltage (Version A/B)


R1245x00xA/R1245x00xB
Vout=5.0V


R1245x00xA/R1245x00xB
Vout $=15 \mathrm{~V}$


R1245x00xA/R1245x00xB
Vout=3.3V
( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


R1245x00xA/R1245x00xB
Vout $=12 \mathrm{~V}$


R1245x00xA/R1245x00xB
Vout $=24 \mathrm{~V}$
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$


## 26) Output current vs. Output voltage (Version C/D)



R1245x00xC/R1245x00xD
Vout=5.0V


R1245x00xC/R1245x00xD
Vout=15V


## R1245x00xC/R1245x00xD

Vout=3.3V


R1245x00xC/R1245x00xD
Vout $=12 \mathrm{~V}$


## R1245x00xC/R1245x00xD

Vout $=24 \mathrm{~V}$


## R1245x

No. EC-269-200624
27) Output current vs. Output voltage (Version E/F)




## R1245x00xE/R1245x00xF

Vout=15V
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$

R1245x00xE/R1245x00xF
Vout $=24 \mathrm{~V}$

28) Output current vs. Output voltage (Version G/H)




## R1245x

No. EC-269-200624
29) Input voltage vs. Output voltage (Version A/B)

30) Input voltage vs. Output voltage (Version C/D)





## R1245x

No. EC-269-200624
31) Input voltage vs. Output voltage (Version E/F)

R1245x00xE/R1245x00xF
Vоит $=0.8 \mathrm{~V}$


R1245x00xEIR1245x00xF
Vout $=5.0 \mathrm{~V}$


R1245x00xE/R1245x00xF
Vout $=15 \mathrm{~V}$


R1245x00xE/R1245x00xF
Vout=3.3V
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$


R1245x00xE/R1245x00xF
Vout $=12 \mathrm{~V}$


R1245x00xE/R1245x00xF
Vout $=24 \mathrm{~V}$

32) Input voltage vs. Output voltage (Version G/H)

R1245x00xG/R1245x00xH
Vout $=1.5 \mathrm{~V}$


R1245x00xG/R1245x00xH
Vоит $=5.0 \mathrm{~V}$


## R1245x00xG/R1245x00xH

Vout $=3.3 \mathrm{~V}$


R1245x00xG/R1245x00xH
Vout $=12 \mathrm{~V}$


The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following conditions are used in this measurement.

## Measurement Conditions

|  | Ultra High Wattage Land Pattern |
| :---: | :---: |
| Environment | Mounting on Board (Wind Velocity $=0 \mathrm{~m} / \mathrm{s}$ ) |
| Board Material | Glass Cloth Epoxy Plastic (Four-Layer Board) |
| Board Dimensions | $76.2 \mathrm{~mm} \times 114.3 \mathrm{~mm} \times 0.8 \mathrm{~mm}$ |
| Copper Ratio | Outer Layers (First and Fourth Layers): $95 \%$ of 50 mm Square <br> Inner Layers (Second and Third Layers): $100 \%$ of 50 mm Square |
| Through-holes | $\phi 0.4 \mathrm{~mm} \times 21 \mathrm{pcs}$ |

Measurement Result
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Tjmax}=150^{\circ} \mathrm{C}\right)$

|  | Ultra High Wattage Land Pattern |
| :---: | :---: |
| Power Dissipation | 3.6 W |
| Thermal Resistance | $\theta \mathrm{ja}=\left(150-25^{\circ} \mathrm{C}\right) / 3.6 \mathrm{~W}=35^{\circ} \mathrm{C} / \mathrm{W}$ |
|  | $\theta \mathrm{jc}=10^{\circ} \mathrm{C} / \mathrm{W}$ |



Power Dissipation vs. Ambient Temperature


Measurement Board Pattern


HSOP-8E Package Dimensions

* The tab on the bottom of the package shown by blue circle is a substrate potential (GND). The tab must be connected to the ground plane on the board.

The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following conditions are used in this measurement.

## Measurement Conditions

|  | Standard Test Land Pattern |
| :---: | :---: |
| Environment | Mounting on Board (Wind Velocity $=0 \mathrm{~m} / \mathrm{s}$ ) |
| Board Material | Glass Cloth Epoxy Plastic (Double-Sided Board) |
| Board Dimensions | $40 \mathrm{~mm} \times 40 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ |
| Copper Ratio | Top Side: Approx. $50 \%$ |
| Bottom Side: Approx. $50 \%$ |  |
| Through-holes | $\phi 0.54 \mathrm{~mm} \times 30 \mathrm{pcs}$ |

## Measurement Result

$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Tjmax}=150^{\circ} \mathrm{C}\right)$

|  | Standard Test Land Pattern |
| :---: | :---: |
| Power Dissipation | 1100 mW |
| Thermal Resistance | $\theta \mathrm{ja}=\left(150^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right) / 1.1 \mathrm{~W}=114^{\circ} \mathrm{C} / \mathrm{W}$ |



Power Dissipation vs. Ambient Temperature


Measurement Board Pattern


DFN2020-8 Package Dimensions (Unit: mm)

* The tab on the bottom of the package shown by blue circle is a substrate potential (GND). The tab must be connected to the ground plane on the board.

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[^0]:    ${ }^{\star 1}$ Connect the backside heat radiation tab to GND or same as GND level (recommendation). The tab is connected to the GND pin.

[^1]:    ${ }^{* 2}$ Connect the backside heat radiation tab to GND or same as GND level (recommendation). The tab is connected to the GND pin.

